

Enhanced Temperature Sensing by Multi-Mode Coupling in an On-Chip Microcavity System

Xueyi Wang, Tingge Yuan, Jiangwei Wu, Yuping Chen,* and Xianfeng Chen

The microcavity is a promising sensor platform, but any perturbation will disturb its linewidth, cause resonance shift or splitting. However, such sensing resolution is limited by the cavity's optical quality factor and mode volume. Here, an on-chip integrated microcavity system is proposed and demonstrated that the resolution of a self-referenced sensor can be enhanced with multi-mode coupling. In experiments, inter-mode coupling strength is carefully optimized with a pulley waveguide and observed a resolution improvement of nearly 3 times in the frequency domain. While experiencing small refractive index change tuned by temperature, mode-coupled system shows a 7.2 times sensitivity enhancement that is than the uncoupled system on the same chip and a very significant lineshape contrast ratio change as great reference for minor frequency shifts. This approach will help design microcavity sensors to improve detection sensitivity and resolution under limited manufacture precision.

1. Introduction

Optical microcavity as one of the building blocks of photonic integrated circuit has enabled a variety of applications including nonlinear optics,^[1,2] low-threshold laser^[3,4] and single molecule detection,^[5–12] its small mode volume and high quality factor (Q factor). Especially in unlabeled sensing^[13–19] or environmental monitoring^[20–25] as a great supplement for medical and environmental research. However, the most adapted sensing scheme

of mode shifting and splitting relies critically on the cavity's Q factor.^[26] Taking the experimental spectral resolution also into account, a 100 million ultra-high Q microcavity can then realize a resolution around 10 fm,^[12] which is yet insufficient for protein detection. On the other hand, a decrease in the cavity's mode volume would increase radiation losses that is no longer neglectable^[27] causing drop in its Q factor. Overcoming such limitation by introducing new principles to microcavity systems thus become urgent. There have been works implementing microcavity lasers^[28,29] to enhance light-matter interaction or by utilizing optomechanical coupling^[30] that boosts sensing resolution by magnitudes.

Among all of the brand new solutions, one of the most approachable is

by introducing mode coupling into the system,^[31] for that it causes little extra fabrication or experiment difficulties. When the two coupled modes are at weak-coupling region,^[32] their coherent interaction can optimize the spectrum's lineshape for efficient sensing.^[33] Within one single cavity, the coupling condition can be satisfied by utilizing modes in different polarization of a micro-toroidal cavity^[34] or by applying UV curable adhesive onto micro-bottle resonator to create a lossy mode,^[35] which achieved a 4.3 times refractive index change sensitivity amplification through its coupling with another discrete mode. Meanwhile, micro-ring resonator is the ideal platform for on-chip integrated sensors, which not only promises giant potential as a built-in sensing component for photonic integrated circuit, but also allows compact, energy-efficient integration of multiple sensors or hybrid sensors with a variety of materials, permitting the simultaneous sensing of multiple analytes or parameters.^[36] With as simple as a built-in Fabry–Pérot (F-P) cavity on its coupled waveguide,^[37] multi-mode coupling between cavities could be achieved. Such structure was first manufactured with polymer platform^[38] that increased the sensitivity of solution refractive index by its sharp resonance slopes, and with a silicon-on-insulator chip as well^[39] which realized a tunable lineshape fitting a variety of applications. Recently, mode coupling has also been controlled by scatterers to function at its exceptional point showing possibility for unprecedented sensitivity.^[40] Thus mode coupling could be a handy improvement to already widely studied microcavity sensors.

In this work, we propose a design method to improve the resolution of microcavity sensors through multi-mode cou-

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Table 1. Previous works with self-referenced photonic thermal sensors.

Year	Material	$dn_1/dT - dn_2/dT$ [K ⁻¹]	Cavity Radius	Sensitivity	Reference
2011	MgF ₂	0.41×10^{-6} @ 1560 nm, 76 °C	4 mm	-89.8 MHzK ⁻¹	[41]
2012	MgF ₂	0.35×10^{-6} @ 1560 nm, 40 °C	3.25 mm	67 MHzK ⁻¹	[42]
2012	MgF ₂	0.54×10^{-6} @ 972 nm, 20 °C	2 mm	-0.17 GHzK ⁻¹	[43]
2014	CaF ₂	-11.4×10^{-6} @ 1064 nm, 532 nm	5 mm	-97.42 MHzK ⁻¹	[44]
2017	LN	-3.7×10^{-5} @ 1523 nm, 50 °C	25 μm	-0.834 GHzK ⁻¹	[45]
2018	LN	-3.34×10^{-5} @ 1560 nm, 26 °C	4.75 mm	3.0 GHzK ⁻¹	[46]
2023	LN	~	129.03 μm racetrack	5.49 GHzK ⁻¹	This work
			129.03 μm ring	0.76 GHzK ⁻¹	This work

pling with a compact, on-chip integrated micro-cavity system. Based on a waveguide to micro-racetrack structure supporting three resonance modes simultaneously and a pulley coupler with careful geometrical optimization, our design allows efficient and distinct inter-mode coupling at 1520 to 1555 nm band for both racetrack quasi-TE and TM modes leading to frequency shifts and sharp lineshape, which helps to distinguish two modes during self-referenced sensing and breaks the sensitivity's dependence on the Q factor that microcavity sensors always suffer from. In frequency domain we achieved three times enhancement in resolution and a sensitivity of 44 pm°C⁻¹ that is not only 7.2 times higher than the uncoupled structure on the same chip, but also excels previous works in self-referenced thermal sensors^[41–46] as shown in **Table 1**. And its lineshape contrast ratio (LCR) offers 24.1 times enhancement in the same time which function as great reference for minor turbulence. Our proposed approach will benefit applications in optical sensors that require integration and high sensitivity probing weak signals under a compromised fabrication efficiency.

2. Theory

Conventionally, when two modes are weakly coupled, for instance one discrete mode and one continuous mode, the discrete mode would experience a frequency shift and linewidth sharpening determined by their detuned wavelength and coupling strength.^[32] While the coupling includes two discrete modes simultaneously, it is very likely that they will experience different shifts for that they possess distinct coupling strength and eigenfrequencies. Thus by controlling the composition of three modes, we could manipulate the relative frequency difference of them after coupling happened, that in certain scenarios would help us to distinguish two discrete modes with higher resolution. Here, we first introduce the theory and how it compose with our on-chip system.

In the waveguide micro-ring resonator (WGMRR) three modes co-exist in the system as in **Figure 1a**, one waveguide (WG) mode reflected by built-in gratings, two micro-ring resonance (MRR) modes with quasi-TE and TM polarization. They possess different coupling efficiency κ_j , internal loss γ_j and resonant frequency separately ω_j ($j = 0$ for WG mode and $j = 1, 2$ for MRR quasi-TE, TM modes respectively as shown in **Figure 1a**).

The system Hamiltonian should be,

$$H_{SYS} = \sum_{j=0,1,2} \hbar \omega_j a_j^\dagger a_j + i \hbar \kappa_1 (a_0^\dagger a_1 - a_1^\dagger a_0) + i \hbar \kappa_2 (a_0^\dagger a_2 - a_2^\dagger a_0) - i g \hbar (a_1^\dagger a_2 - a_2^\dagger a_1) \quad (1)$$

In which $a_j^\dagger$ (a_j) are photon creation (annihilation) operators. For the oblique nature of the side walls ridge waveguide and birefringence of X-cut LN (Lithium Niobate), the quasi-TE (TM) modes are not perfectly parallel (vertical) to the substrate plane (see inset of **Figure 1a**; Section **S1.1**, Supporting Information) which causes them to couple with a coefficient g .^[48] At the same time enabling WG TE₀₀ photon a_0 to generate MRR TM mode a_2 with different polarization. Similarly, at the time a_2 couples back into the waveguide it is projected into TE polarized beams that lead to its coherent interaction with a_0 lights.

Under the first Markov approximation $\kappa_0^2(\omega) = \kappa_0/2\pi$,^[49] we approach the Langevin equations of motion as follow,

$$\begin{pmatrix} \dot{a}_0 \\ \dot{a}_1 \\ \dot{a}_2 \end{pmatrix} = \begin{pmatrix} -i\omega_0 - \frac{\kappa_0 + \gamma_0}{2} & \kappa_1 & \kappa_2 \\ -\kappa_1 & -i\omega_1 - \frac{\kappa_1 + \gamma_1}{2} & -g \\ -\kappa_2 & g & -i\omega_2 - \frac{\kappa_2 + \gamma_2}{2} \end{pmatrix} \begin{pmatrix} a_0 \\ a_1 \\ a_2 \end{pmatrix} + \begin{pmatrix} \sqrt{\kappa_0} a_{IN} \\ 0 \\ 0 \end{pmatrix} \quad (2)$$

$a_{IN} = \sqrt{2P_{IN}\kappa_0/\hbar\omega_0}$ is the input amplitude in TE polarization and so as a_0 . Then we solve Equation (2) in frequency domain,

$$(\omega - \tilde{\omega}_0)a_0 = -i\kappa_1 a_1 - i\kappa_2 a_2 - i\sqrt{\kappa_0} a_{IN} \quad (3)$$

$$(\omega - \tilde{\omega}_1)a_1 = i g a_2 + i \kappa_1 a_0 \quad (4)$$

$$(\omega - \tilde{\omega}_2)a_2 = -i g a_1 + i \kappa_2 a_0 \quad (5)$$

in which $\tilde{\omega}_j = \omega_j - i \frac{\kappa_j + \gamma_j}{2}$ ($j = 0, 1, 2$) is the complex eigenfrequency. Equation (3) implies that the output field is made up by the coherent superposition of a_1, a_2 , to a_0 mode with coupling constant κ_1 and κ_2 , respectively. In weak coupling region, the coupling strength need to be comparable to the modes' dephasing rate to appear in the transmission spectrum of the system,^[32]

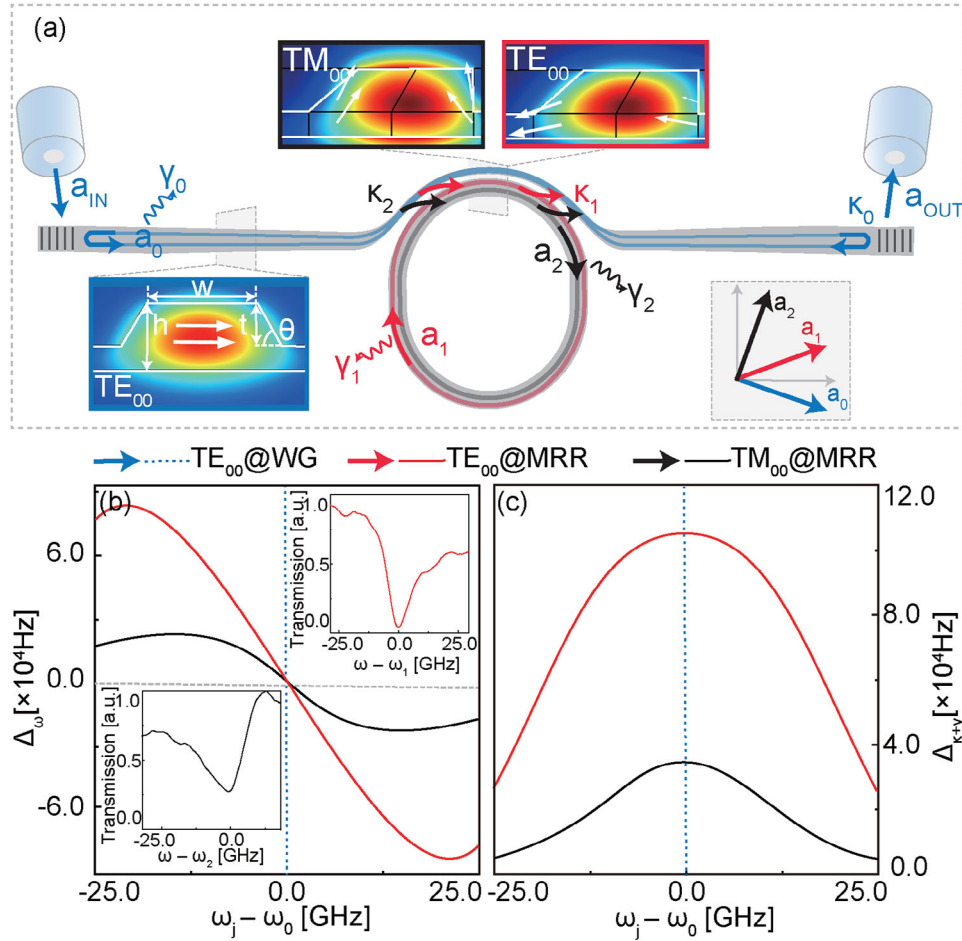


Figure 1. a) Scheme of the WGMR system with WG mode in blue and MRR quasi-TE and quasi-TM in red and black, respectively. The insets are calculated with conformal transformation^[47] indicating the polarization of TE₀₀ and TM₀₀ in straight and curved waveguides (see also Section S1.1, Supporting Information). Frequency shift b) and linewidth sharpening c) for different MRR modes caused by coupling, insets are transmission spectrum of quasi-TE, TM modes after coupling.

since the inter-modal coupling coefficient g within the MRR is minor compared to κ_1 and κ_2 , the output amplitude $a_{OUT} = \sqrt{\kappa_0}a_0 - a_{IN}$ approximates to,

$$a_{OUT} = \kappa_0 \xi a_{IN} - a_{IN} \quad (6)$$

$$\xi = \frac{i(\omega - \tilde{\omega}_1)(\omega - \tilde{\omega}_2)}{(\omega - \tilde{\omega}_0)(\omega - \tilde{\omega}_1)(\omega - \tilde{\omega}_2) - \kappa_1^2(\omega - \tilde{\omega}_2) - \kappa_2^2(\omega - \tilde{\omega}_1)} \quad (7)$$

the transmission spectrum should be,

$$T = \left| \frac{a_{OUT}}{a_{IN}} \right|^2 \approx 1 - 2\kappa_0 \xi \quad (8)$$

where $|\kappa_0 \xi|^2$ is ignored in above equation. Solving the denominator of ξ there are (details in Section S2, Supporting Information),

$$\tilde{\omega}_{j\pm} = (\tilde{\omega}_0 + \tilde{\omega}_j \pm \delta_j)/2, \delta_j^2 = (\tilde{\omega}_0 - \tilde{\omega}_j)^2 + 4\kappa_j^2 \quad (9)$$

the eigenfrequencies of MRR are shifted by complex frequencies $\tilde{\Delta}_{\pm j} = \tilde{\omega}_{j\pm} - \tilde{\omega}_j = (\tilde{\omega}_0 - \tilde{\omega}_j \pm \delta_j)/2$, (+ : $\omega_0 - \omega_j > 0$, - : $\omega_0 - \omega_j < 0$) respectively, in which $\Delta_\omega = \text{Re}(\tilde{\Delta}_{\pm j})$ stands for shifts in frequency and $\Delta_{\kappa+j} = -\text{Im}(\tilde{\Delta}_{\pm j})$ for changes in linewidth. Consequently, MRR modes experience a red (blue) shift if they are blue (red) detuned to ω_0 and a linewidth reduction either way as shown in Figure 1b,c. For that quasi-TE mode has greater κ that leads to bigger $|\Delta_\omega|$ and $|\Delta_{\kappa+j}|$ for a_1 .

Consequently, if two MRR modes locate across the continuum mode eigenfrequency they would be “pulled closer” as their frequencies are shifted towards each other $|\Delta'_{12}| = |\Delta_{12}| - [| \text{Re}(\delta_1) | + | \text{Re}(\delta_2) |]/2$ as case I in Figure 2a. Or they could be “pushed apart” if coupled to two different continuum modes as the cases in Figure 2a II. that $|\Delta'_{12}| = |\Delta_{12}| + [| \text{Re}(\delta_1) | + | \text{Re}(\delta_2) |]/2$. In the case when their frequency differs even less, within one side of the background’s FSR (free spectrum range), then they are “pushed apart” when mode with larger κ locates closer to ω_0 only then $|\Delta'_{12}| = |\Delta_{12}| + [| \text{Re}(\delta_1) | - | \text{Re}(\delta_2) |]/2$ could be enlarged (as the case in Figure 2a III, the width of modes’ stripes indicates their relative coupling strength), and “pulled

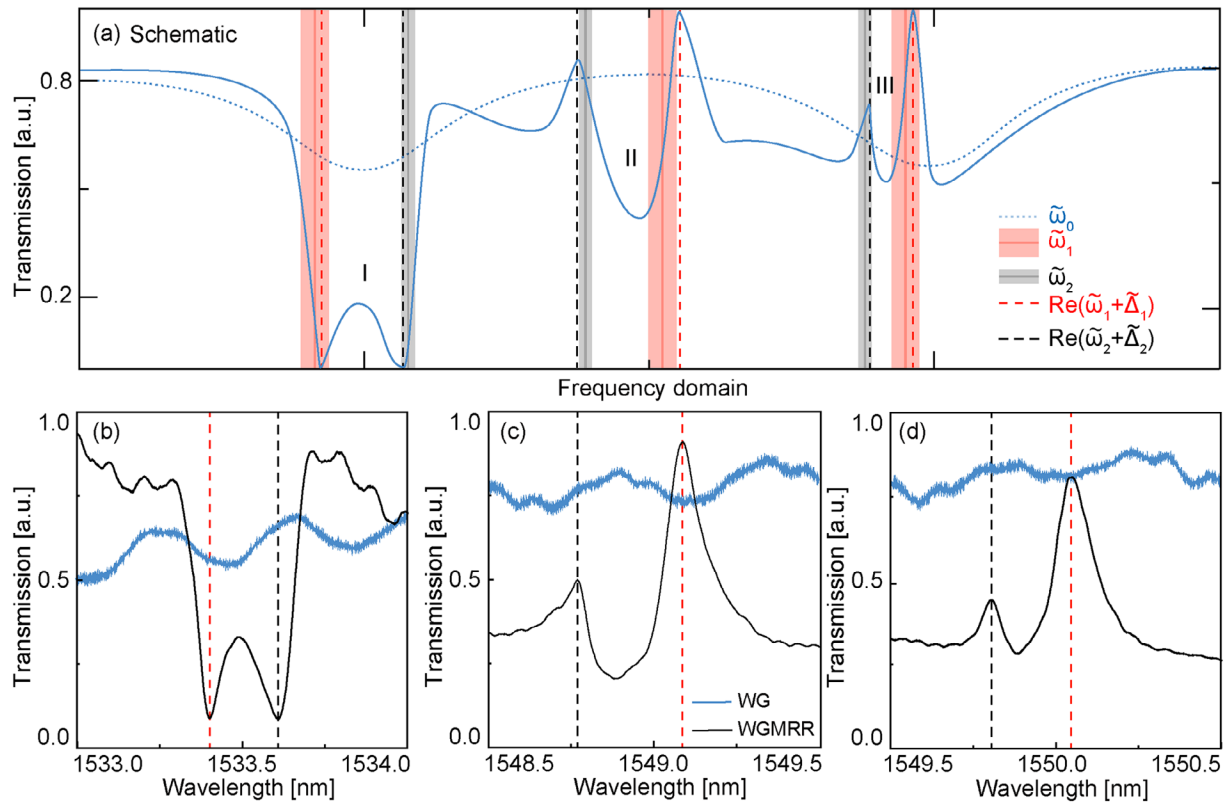


Figure 2. a) Schematic of the proposed mode coupling involving three modes arranged in three fashions leading to different mode resolution: when MRR modes locate I across background eigenmode then they are “pulled closer”, II over different background eignmodes and III within one side of background mode while mode with larger κ is closer to ω_0 when they are “pushed apart”, wider stripe indicates stronger coupling strength of the eigenmode to the background mode. Transmission spectrum of the WGMRR and WG in black and blue which satisfies the above scheme I b), II c), and III d) respectively.

closer” if in the opposite case. Under the circumstances when multi-mode coupling leads to “pushed apart”, it enhances the observation resolution of two adjacent MRR modes, which is ideal for sensing applications or mode measurements. From our following experiments, clearly in Figure 2b,c,d the transmission spectrum of the WGMRR and WG (in black and blue) has strongly asymmetric dips and peaks indicate multi-mode coupling happening in the above (I to III) scenarios.

3. Results

3.1. Experimental Setup

The experimental setup is in Figure 3a, it involves a tunable infrared laser source (New Focus TLB-6728) which is adjusted by a PC (polarization controller) and then coupled into the chip through built-in gratings on the waveguide. After the output port

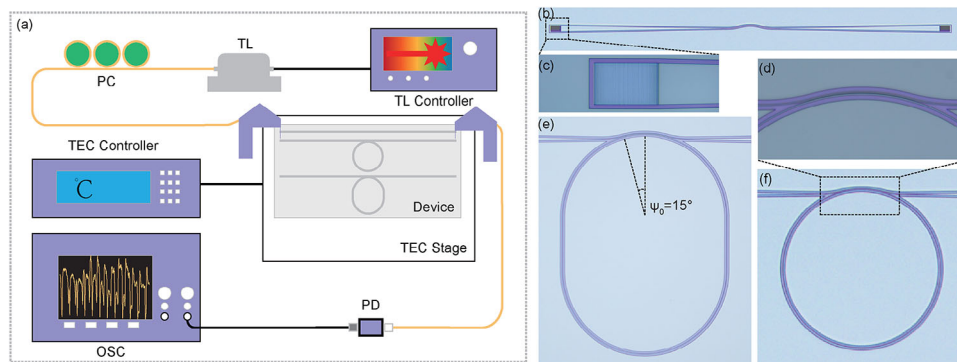


Figure 3. a) Experiment setup. TL: Tunable Laser, PC: polarization controller, PD: photon detector, OSC: oscillator, TEC: thermoelectric cooler, electrical wire and optical fiber in black and yellow, respectively. Microscopic pictures of the single waveguide b), gratings c), coupling region d), racetrack e) and ring f) resonators.

a PD (photodetector) collects the transmission information that is then shown on the OSC (oscilloscope). Meanwhile, the chip is loaded on a TEC (thermoelectric cooler) stage with a precision up to 0.01 degree Celsius. From this setup any multi-mode coupling effect is acquired from the the lineshape of transmission spectrum.

To achieve multi-mode coupling and compare its effects, we integrate a waveguide, a waveguide to micro-ring and a waveguide to micro-racetrack all manufactured on one single X-cut LNOI (lithium niobate on insulator) chip with standard electron beam lithography and plasma-reactive etching (see fabrication details in Section S3, Supporting Information). As marked in insets of Figure 1a, the chip thickness is $h = 0.6 \mu\text{m}$, while top width of waveguide is $w = 1 \mu\text{m}$, thickness $t = 0.38 \mu\text{m}$, and side wall angle $\theta = 60^\circ$, which are ideal to support only fundamental modes. The radius of both micro-racetrack and micro-ring is the same $R = 129.03 \mu\text{m}$ while the racetrack contains an extra straight waveguide of $82.54 \mu\text{m}$ to compose its FSR with the WG modes'. The coupling grating in Figure 3c is of $23 \mu\text{m}$ wide to collect the light spot from a cleaved SMF (single mode fiber) tip sufficiently and the waveguide then slowly shrinks down to the pulley coupler enabling adiabatic coupling.^[50] At the coupling region Figure 3d, the waveguide width shrinks down to $0.8 \mu\text{m}$ with a gap of $G = 0.6 \mu\text{m}$ to achieve sufficient evanescent field coupling, next we calculate such coupling strength and analyze its effect in detail.

3.2. Multi-Mode Coupling in Frequency Domain

From the system Hamiltonian, we could tell that the inter-modal coupling strength is determined by the mode coupling efficient κ at the pulley waveguide, and it can be calculated with temporal perturbation theory as [51] (details in Section S1.2, Supporting Information),

$$\kappa = \int_{-\psi_0}^{\psi_0} \left[\frac{i\omega}{4} \int_0^{R+G} \int_0^t (\epsilon - \epsilon_0) \mathbf{E}_{WG} \cdot \mathbf{E}_{MRR} r dr dz \right] e^{i\varphi} d\psi \quad (10)$$

in which $\mathbf{E}_{WG} \cdot \mathbf{E}_{MRR}$ corresponds to the mode overlap of normalized WG and MRR fields, permittivity ϵ can be obtained from the electric field and is shown in the mode's effective refractive index (n_{eff}) in Figure 4a,b. And $\varphi = k_0 n_{WG} R_{WG} \psi - m\psi$, m is the radial mode number of resonance mode inside cavity, φ reflects the phase mismatch between the waveguide and cavity mode that has major impact on κ . Meanwhile X-cut LN is an anisotropic material as n_{eff} shifts across azimuth angle ψ infecting phase matching condition along its way, thus it introduces change in κ proportional to $\text{sinc}(\varphi)$, see Figure 4c, where κ_{TE} increases and κ_{TM} decrease as ψ grows. It offers another degree of freedom to manipulate coupling strength between different polarization with the angle and length of pulley coupling scheme. Also in frequency domain (Figure 4d) κ degenerates significantly at longer input wavelength due to non-ideal phase matching and mode overlapping, in the following experiments we clearly observed weaker mode coupling at longer wavelength as shown in Figure 4g. Reminding that the pulley waveguide needs to be carefully designed to achieve sufficient coupling at target work waveband. In our design, κ is set to generate sufficient coupling for both polarization

across C-band at the same time differs with nearly one degree of magnitude so they appear with diverse mode shifts during coupling to be distinguished.

With above system we first obtain the transmission spectrum of the micro-racetrack (Figure 4e) the cavity modes preserved a strongly asymmetric lineshape due to the coupling with WG modes (the transmission spectrum of waveguide is in blue). The effective Q factor calculated by applying Lorentz fitting of the dip reaches $Q_E = 11.07k$ and $Q_M = 14.09k$ for TE and TM, respectively. With calculated coupling $Q_{CE} = 17.10k$, $Q_{CM} = 62.31k$ which ends up in coupling coefficients $\kappa_E = 2.67 \times 10^5$, $\kappa_M = 1.40 \times 10^5$ slightly larger than the simulation in Figure 4d supposedly caused by coupling region $\psi > 15^\circ$ which has a larger gap but still allows evanescent field coupling. Compared to their intrinsic Q factors $Q_{0E} = 27.52k$, $Q_{0M} = 18.21k$, the TE modes are over-coupled leading to strong interference by WG modes, theoretically it causes mode shift up to 72.52 kHz as shown in Figure 1b. Experimentally, due to the different FSRs of TE and TM modes, the wavelength difference between two closest modes $|\Delta_{12}|$ would first increase and then decrease to zero during a certain wavelength range as the insets of both Figure 4f,h. In a coupled system, $|\Delta_{12}|$ and modes' FWHM (full width half maximum, w_1, w_2 for TE and TM respectively) were tuned by coupling strength and relative background phase as in Figure 4f, determined by $\tilde{\omega}_0 - \tilde{\omega}_1$ according to Equation (9). The measured degree of mode separation $\frac{|\Delta_{12}|}{(w_1+w_2)/2}$ is enhanced for TM modes with radial mode number 1153 to 1158 (marked in red in Figure 4f), satisfying either scenario II or III from Figure 2a, nearly three times larger compared to their siblings (mode number 1153 to 1163).

Meanwhile, in the uncoupled system with micro-ring resonator (Figure 3e), whose loaded Q factors are $Q'_E = 22.61k$, $Q'_M = 10.76k$ and coupling $Q'_{CE} = 137.37k$, $Q'_{CM} = 203.82k$ that is significantly under-coupled. Calculated from its spectrum Figure 4g the mode separation $\frac{|\Delta_{12}|}{(w_1+w_2)/2}$ is proportional to $|\Delta_{12}|$ despite of the fluctuation in FWHM caused by coupling depth as in Figure 4h showing no signs of resolution enhancement nor inter-mode coupling. Next we run tests over their sufficiency of detecting minor temperature shifts for both systems.

3.3. Temperature Sensing Enhanced by Multi-Mode Coupling

In previous works utilizing double mode coupling such as fano resonance for sensing purpose, apart from the sharp asymmetric lineshape that declines the effective mode linewidth, those two modes are self-referenced so the system accuracy is no longer limited by experiment equipment.^[35] According to above analysis, MRR quasi-TE and TM modes would sufficiently form a self-referenced sensing system while coupling with WG mode further improves its capacity. Here, to compare the sensitivity for weak turbulence of a mode-coupled and an uncoupled system, we keep the laser source sweeping in wavelength and slightly adjust the stage's temperature control which tunes n_{eff} of the MRR consequently. At around 1550 nm wavelength the micro-racetrack forms an EIT-like spectrum in Figure 5a, the three groups of modes experienced different shifts due to their coupled background phase, the gap between two closest modes $|\Delta_{12}|$ shifts as large as $44 \text{ pm}^\circ\text{C}^{-1}$ which is 7.2 times larger than the uncoupled

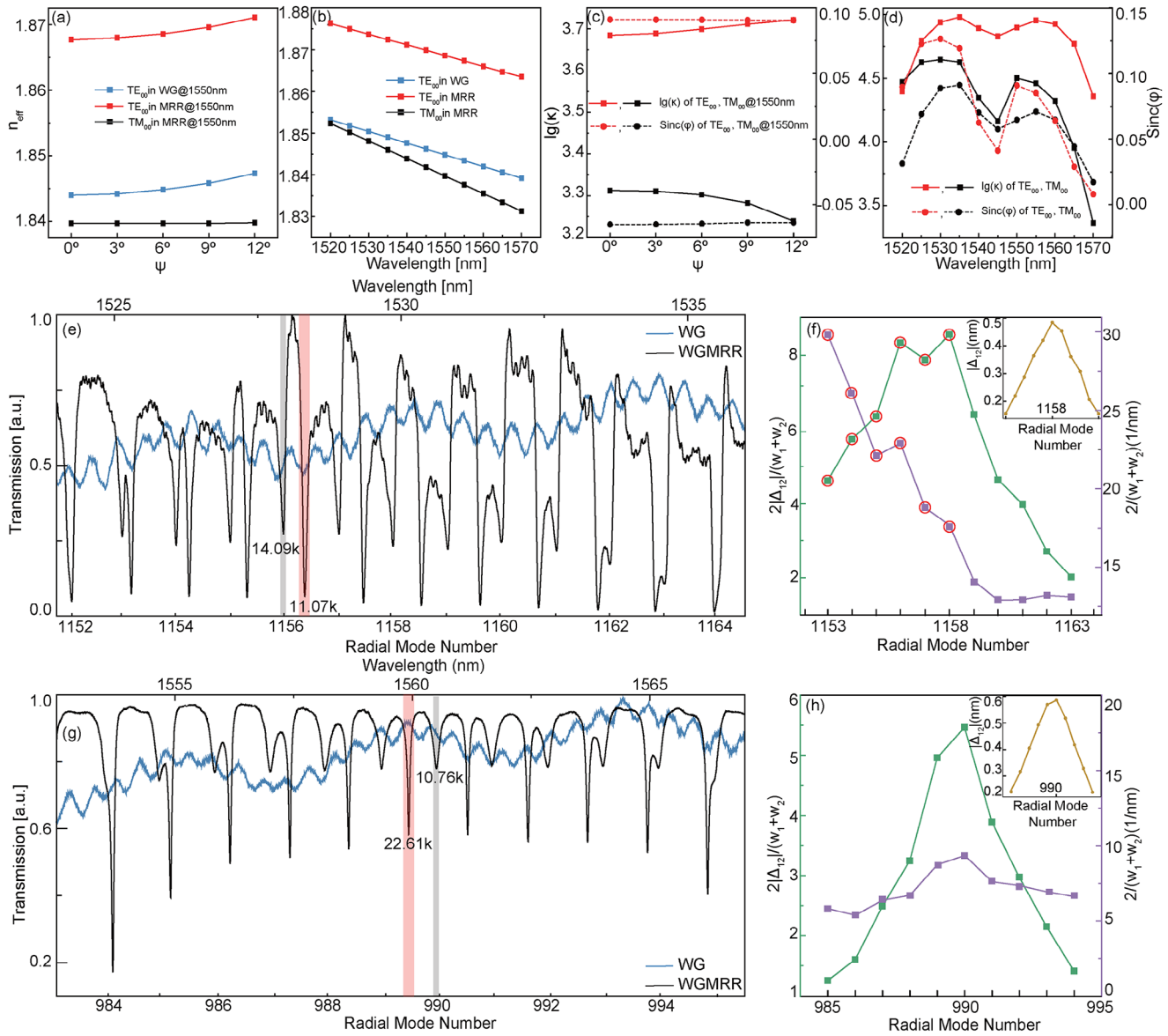


Figure 4. The simulated effective refractive index (n_{eff}) at different angles a) on the X-cut LN chip and across resonance wavelength b). Coupling coefficient $\lg(k)$ and $\text{sinc}(\varphi)$ at different angles c) on the X-cut LN chip and across resonance wavelength d). e) Transmission spectrum of the WG-micro-racetrack and the sole waveguide (in blue) when there is multi-mode coupling. g) Transmission spectrum of the WG-micro-ring and the sole waveguide (in blue) when there is no multi-mode coupling. Measured wavelength difference $|\Delta_{12}|$, FWHM $2/(\omega_1 + \omega_2)$ and their product $2|\Delta_{12}|/(\omega_1 + \omega_2)$ declaring the degree of mode separation of TM mode and its closest TE mode in frequency domain for coupled f) and uncoupled h) system, the red circle marks where inter-modal separation is significantly enlarged by coupling.

system in Figure 5b that has very similar mode gaps in the first place, as shown in Figure 5c. Despite the fact that under the same circumstances, a smaller cavity with a larger FSR theoretically brings about higher sensitivity for shifts in the cavity's refractive index δn , its corresponding wavelength shift approximates to $\delta\lambda \approx \frac{\delta n}{n_{eff}} \times \text{FSR}$.^[6]

On the other hand, a mode-coupled system possess a lineshape sensitive to its background phase.^[52] In our setup the background modes have a linewidth of 0.23 nm and FSR of 0.45 nm (and it is also insensitive to thermal changes, see Section S4, Support-

ing Information), thus even a minor shift at $\sim$ pm would lead to observable changes to the spectrum lineshape. That experiences a change in its LCR ($\frac{(I_1 - I_0) + (I_2 - I_0)}{I_1 + I_2}$) as large as $6.46 \times 10^{-3} \text{ pm}^{-1}$, while the according uncoupled modes only changes $0.27 \times 10^{-3} \text{ pm}^{-1}$ as in Figure 5d. So there is a maximum 24.1 times enhancement compared with the uncoupled spectrum at similar temperature working as another crucial criterion for minor turbulence in the system's n_{eff} . Meanwhile, the multi-mode coupling effect of our device is proved to be robust in a wide temperature range from 15 to 80 °C as the furthest the TEC stage could reach and

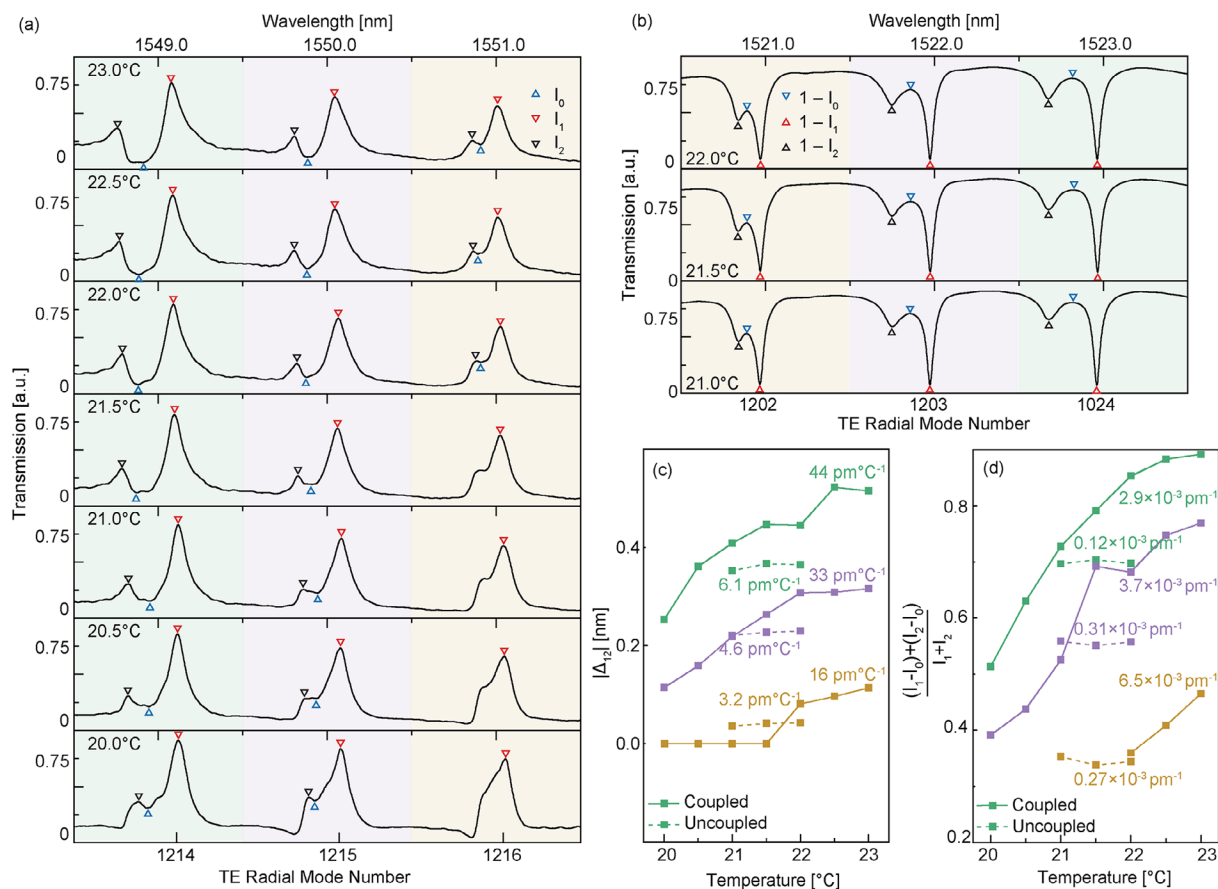


Figure 5. a) Transmission spectrum the WGMRR with multi-mode coupling leading to “pushing apart”. b) Transmission spectrum of the WGMRR without mode coupling by adjusting input polarization and wavelength. c) Measured wavelength separation $|\Delta_{12}|$ of a) and b) (dashed) at different temperature. d) Calculated lineshape contrast ratio $\frac{(I_1-I_0)}{(I_1+I_2)}$ of a) and b) (dashed), under multi-mode coupling their lineshapes experience a contrast shift 24.1 times greater.

so does its sensing capability (details in Section S5, Supporting Information).

However, both of the sensing results we have discussed above show a degree of saturation as the temperature shifts larger, for one single group of modes, the enhanced sensing scheme has a range determined by the WG modes' FSR, which approximates to 10.2 °C for scheme II and 6.8 °C for scheme III based on our experiments in Figure 5. Also, it is still worth noting that our design did not reach the best performance among all of the microcavity thermal sensors. Apart from the fact that our on-chip microcavities were built large in the first place to compensate the WG mode's FSR, the pulley waveguide was designed to reach over-coupling condition that leads to decrease in MRR modes' Q factor and coupling depth. Taking those information under consideration, a further improvement should utilize the coupling of multiple high- Q factor modes either by connecting several micro-resonators^[31] or by optimizing cavities that support a number of resonance modes.

4. Conclusion

In this paper, we have in depth analyzed dimensions of multi-mode coupling, revealing the intrinsic connection between

frequency, Q factor enhancement and modes' composition. Based on theoretical discussions and experiments demonstrated with an on-chip integrated WGMRR, we have achieved higher resolution in frequency domain and improved sensitivity as a self-referenced sensor with micro-racetrack's quasi-TE and TM modes coupled to waveguide resonance mode at the same time. Here, we have confined our discussions of mode-coupled sensors within the fundamental case, practiced between discrete and continuum modes, and it is expected that a natural extension to more sophisticated configurations with several high- Q modes or even multiple exceptional points would reach much higher magnitudes of enhancement for microcavity sensors without over-investing into manufacture techniques. Though our design was practiced with a LNOI micro-racetrack, we believe that this method can be applied to any cavity-based sensors or other material platforms with great integration capability.

Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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Conflict of Interest

The authors declare no conflict of interest.

Data Availability Statement

The data that support the findings of this study are available from the corresponding author upon reasonable request.

Keywords

integrated optics, micro-optical device, mode coupling, optical sensing and sensors, resonant modes

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