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## Research Article

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## Response Times of Degenerately Doped Semiconductor Based Plasmonic Modulator

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**Abstract:** We present a transient response study of a semiconductor-based plasmonic switch. The proposed device operates through active control and modulation of localized electron density waves i.e., Surface Plasmon Polaritons (SPPs) at degenerately doped  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  based  $\text{PN}^{++}$  junctions. A set of devices are designed and fabricated, and their optical and electronic behaviors are studied both experimentally and theoretically. Optical characterization shows far-field reflectivity modulation, a result of electrical tuning of the SPPs at the  $\text{PN}^{++}$  junctions for mid-IR wavelengths with significant 3dB bandwidths. Numerical studies using a self-consistent electro-optic multi-physics model are performed to uncover the temporal response of the devices' electromagnetic and kinetic mechanisms facilitating the SPP switching at the  $\text{PN}^{++}$  junctions. The numerical simulations show strong synergy with the experimental results, validating the claim of possible electrical tunability of the device with a 3dB bandwidth as high as 2GHz. Thus, this study confirms that the presented SPPD architecture can be implemented for high-speed control of SPPs through electrical means, potentially providing a pathway toward fast all-semiconductor plasmonic devices.

**Keywords:** Optoelectronics, Plasmonics, Surface Plasmon Polariton, PN Junction

## **Introduction:**

To realize nanoscale integrated opto-electronic logic circuits, subwavelength confinement of light and integration of photonic devices with nanoscale electronics are indispensable [1-6]. In this context, the field of plasmonics opens a wide range of possibilities to design subwavelength, high speed, and high efficiency optical devices [7-20]. It is now well recognized by the research community that plasmonics provides possible solutions for integration between nano scale electronic and photonic components on a single chip, paving a new path toward optoelectronic devices characterized by fast information transfer and data processing [21-23]. Such capabilities can be accomplished through the excitation of Surface Plasmon Polaritons (SPPs), a collective excitation of electrons occurring at the interface between a metal/doped semiconductor and a dielectric medium [24]. Most importantly, the SPPs' exceptional spatial confinement at the metal-dielectric interface suggests them as one of the ideal candidates for the prospect of nanoscale chip level interconnects with spatial dimensions compatible with that of nanosized electronic devices.

Over the last few decades, due to advances in electromagnetic simulations and nanofabrication techniques, SPPs have attracted researchers resulting in a surge of progress towards promising applications such as super lenses [25, 26], light harvesting [27-28], metamaterials [29-32], plasmonic enhanced optoelectronics devices [33-38], and waveguiding and switching of SPPs [39-53]. In the context of plasmonic-based optoelectronic elements, so far, it has been showed that SPPs can be modulated at rates from a few kHz [54] to tens of MHz [43-45] and into the GHz range [55, 56]. Here, most of the reported works on SPP modulation use metal-dielectric structures. Metal-based optoelectronic devices can be applied toward integrated optical circuits if the device can successfully address the following challenges. First, common metals such as gold or silver have plasma frequency in the blue or deep ultra-violet wavelength ranges. There

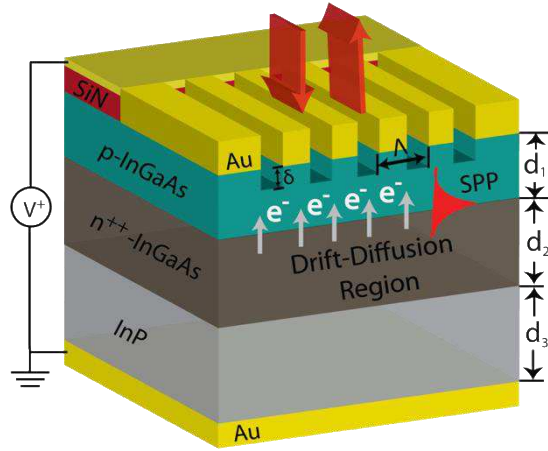
are no available metals whose plasmon resonances are in the near or mid-infrared (MIR) wavelength range which is a highly useful wavelength range for detection and sensing applications [57, 58]. Second, large losses associated with metals stands as a key problem hindering the widespread implementation of metal-based architectures for many plasmonic and metamaterial applications. In addition, the plasma frequency for a given metal is fixed. Thus, there is no notable tunability offered by metal-dielectric structures that could benefit a variety of applications. New exciting physics behavior and applications of SPP based devices can arise if the dissipative losses in the metal-based plasmonic structures are reduced and a pathway toward integration with the current semiconductor technology is provided [59]. Such capabilities can be achieved if plasmonic devices are built based on highly doped semiconductors instead of conventional metals such as gold and silver. This is because heavily doped semiconductors can exhibit a small negative permittivity, low loss, and the potential for integration with semiconductor based electronic and optoelectronic devices [60-61]. It is also worth mentioning that while the field of metal based plasmonics is currently a mature discipline, the area of semiconductor based plasmonics is still rapidly developing.

In this work, we present a significant step towards realizing a complete semiconductor-based plasmonic switch referred to as a Surface Plasmon Polariton Diode (SPPD) [62-65]. Here, we build upon our past work [65], where we have demonstrated excitation and modulation of SPPs modes at the interface of the degenerately doped lattice-matched Indium Gallium Arsenide ( $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ )  $PN^{++}$  - junctions grown epitaxially on Indium Phosphide (InP) and proceed to the next important step by experimentally demonstrating the temporal response of the device. Small signal frequency response measurements are performed, clearly demonstrating frequency dependent optical modulation (switching) of SPP modes at the  $PN^{++}$  junction. Furthermore, to

explore the factors determining the modulation speed of the SPPD, we employ an electro-optic Multiphysics numerical model, which self-consistently solves the  $PN^{++}$  junctions drift-diffusion equations at finite temperature (Fermi-Dirac statistics). The developed model provides accurate simulations of the local charge carrier dynamics, changes in the  $PN^{++}$ - junction capacitance and electro-optical modulation of the local charge density waves as a function of applied input signal voltage and wavelength. The theoretically performed small signal analysis correlates well to our experimental data, attesting to the potential of the proposed device architecture as an excellent electro-optic plasmonic switch. Moreover, our time dependent studies validates that the presented device architecture is capable of operating at 3dB bandwidths of up to 40MHz and, by scaling down the device spatial dimensions, can reach response times as high as 2GHz.

The presented device in this work, an all-semiconductor plasmonic switch, uses an  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  based  $PN^{++}$ - diode. The diode is structured as a heavily doped  $P$ - layer and degenerately doped  $N^{++}$ - layer grown on Indium Phosphide (InP) and with active drift-diffusion region formed between an anode (top grating electrode) and a cathode (bottom contact). A schematic of the device is shown in Figure 1. The state of the device is considered ‘ON’ under zero external bias. The device architecture depicts a scenario of a “metal”-dielectric interface, where the heavily doped  $P$ - layer acts as a dielectric and the degenerately doped  $N^{++}$ - layer acts as a metal, thus supporting excitation of SPP modes at the  $PN^{++}$ - interface. To excite the SPP modes we use a grating coupling technique; where transverse magnetic (TM) polarized radiation is coupled to the SPPs at the interface via a grating. Under the presence of sufficient external forward bias voltage  $V$ , the charge carriers in  $N^{++}$ - doped layer gain enough energy to surpass the potential barrier provided by the  $PN^{++}$ - depletion region and are injected into the  $P$ - doped region. This charge injection process results in modifying the  $P$ -layer’s permittivity  $\epsilon_p$ . When applying external

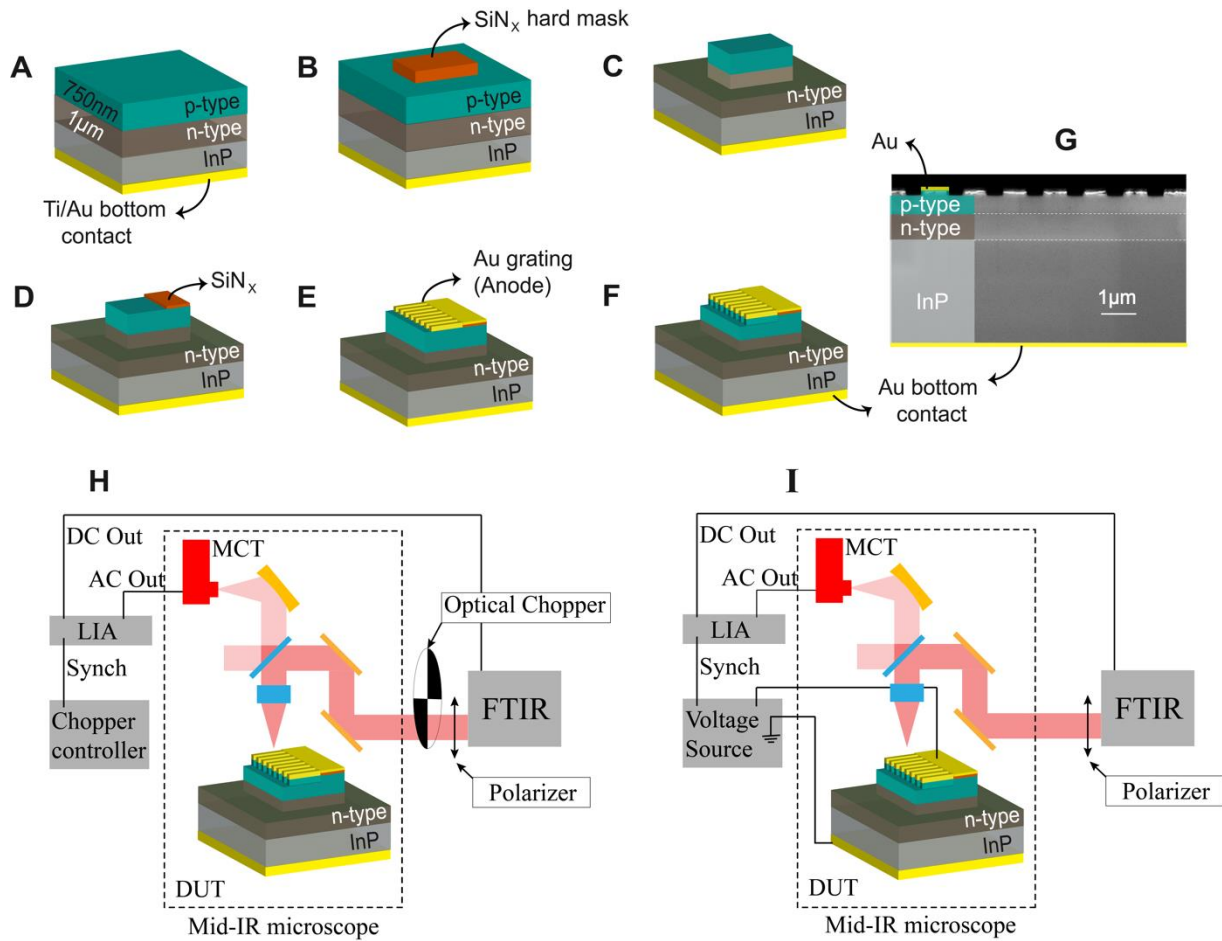
bias  $V > V_c$ , where  $V_c$  is a critical voltage [65], some portion of the  $P$ -layer can acquire metal-like characteristics with  $\epsilon_p < 0$ , which results in hindering the propagation of the SPP modes within the active drift-diffusion region. This state of the device is considered as the ‘OFF’ state.



**Figure 1** Basic architecture of Surface Plasmon Polariton Diode (SPPD), consisting of lattice matched Indium Gallium Arsenide ( $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ )  $\text{PN}^{++}$ -junction grown epitaxially on an Indium Phosphide (InP) substrate. A grating with period  $\Lambda = 2.4 \mu\text{m}$  and  $P$ -layer etch depth of  $\delta = 260\text{nm}$  are used to couple infrared incident light to the SPP modes to the  $\text{PN}^{++}$ -junction. The relevant device sizes are as follows;  $d_1 = 0.75 \mu\text{m}$ ,  $d_2 = 1 \mu\text{m}$ ,  $d_3 = 500 \mu\text{m}$ .

The SPPD is fabricated from an epitaxially-grown Indium Gallium Arsenide ( $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ )  $\text{PN}^{++}$  junction lattice-matched to an Indium Phosphide (InP) substrate, with doping concentrations  $N_D = 3.4 \times 10^{19}\text{cm}^{-3}$  and  $N_A = 1 \times 10^{18}\text{cm}^{-3}$ , respectively. The device fabrication process flow is shown in Figure 2. The fabrication begins with the metallization (Ti/Au, 10/500 nm) of the backside of a wafer to form the bottom electrode. A 640 nm silicon nitride layer was next deposited on the device top surface using plasma enhanced chemical vapor deposition (PECVD,  $\text{NH}_3/\text{N}_2/\text{SiH}_4$ , 10/500/40 sccm). The silicon nitride layer was then patterned into mesas

( $700\mu\text{m} \times 600\mu\text{m}$ ) by UV lithography and dry etching using an Oxford80 reactive ion etcher (RIE) ( $\text{CHF}_3/\text{O}_2$ , 20/4 sccm). The patterned silicon nitride serves as an etch mask for the device mesas formed by dry etching using an Oxford100 inductively coupled plasma (ICP) system ( $\text{Cl}_2/\text{CH}_4/\text{H}_2$ , 6/4/7 sccm). Mesas were etched to a depth of 1300nm. The silicon nitride residue was then cleaned by buffered oxide etch (BOE). A 350 nm PECVD-deposited silicon nitride layer is then patterned to serve as an electrical isolation pad ( $280\mu\text{m} \times 600\mu\text{m}$ ) on the top of the mesa structures. The device top contact, comprising a bond pad above the silicon nitride isolation pad and a grating structure contacting the top surface is shown in insert of Figure 5A, which is fabricated by UV lithography, metal deposition (Ti/Au, 10/250 nm) and lift-off. Finally, we performed another ICP dry etch to form the grating structure (etching to a depth of 260 nm) in the top p-InGaAs, using the top grating contact as a hard mask. During the dry etch, the top Au contact was etched 120nm, with the remainder of the sample protected by photoresist, and later cleaned by oxygen plasma. The sample was then mounted on copper blocks with indium paste and the top contact was wire-bonded to a Pasternack PE4542 SMA connector with ground pins soldered to the same copper block, shown in insert of Figure 5A.



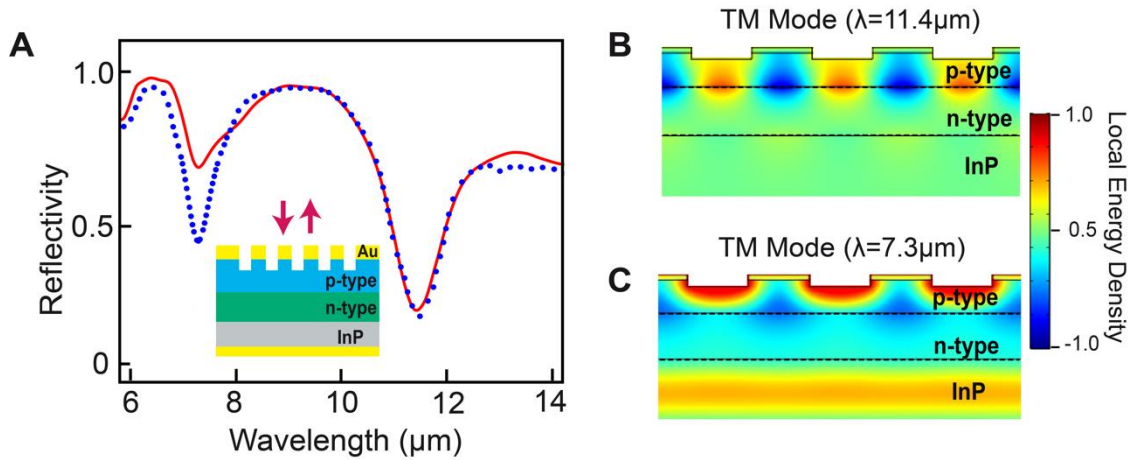
**Figure 2 SPPD fabrication and experimental setup.** (A) Layer structure of the  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$   $\text{PN}^{++}$  diode grown on InP and bottom contact deposition. (B) Device layout after first  $\text{SiN}_x$  deposition and etch mask patterning (C) ICP dry etching to form the mesas on the  $P$ -doped layer, followed by a BOE etch to remove the  $\text{SiN}_x$  hard mask. (D) Second  $\text{SiN}_x$  deposition and patterning to provide an electrical isolation layer. (E) Top metal contact deposition. (F) ICP dry etch of the grating. Experimental set-up for polarization dependent reflectivity measurements under (G) zero voltage bias and (H) under external applied voltage modulation.

Following device fabrication, we performed polarization-dependent reflection spectroscopy using the setup shown in Figure 2H. Light from the internal source of a Bruker v80V Fourier transform infrared (FTIR) spectrometer was sent through a polarizer, modulated by a

mechanical optical chopper, and focused on the grating structures through a mid-IR microscope with a 15x Cassegrain objective. Reflected light was collected by the same objective and detected by the microscope's internal HgCdTe (MCT) detector. The output of the detector was sent to a lock-in amplifier synchronized to the optical chopper. The FTIR was operated in step scan mode, where at each mirror position, the output of the LIA was recorded, giving the interferogram of the reflected signal. The polarization-dependent reflectivity was then obtained by normalizing the sample reflection spectrum to the reflection from a gold surface measured in the same set-up. The transverse magnetic (TM) polarized reflectivity spectra of an unbiased device is shown in Figure 3A, with distinctive dips in reflectivity observed at  $\lambda \sim 7.3 \mu\text{m}$  and  $\lambda \sim 11.4 \mu\text{m}$ . These reflection features correspond to coupling into electromagnetic (EM) modes supported either at the  $PN^{++}$ -interface or in the higher index P-layer of the device. To investigate these spectral features, we modified the already-developed COMSOL-based electro-optic model [62-65] to solve for the current device architecture and proceeded to numerically examine the fabricated SPPD. Essential parameters required to effectivity replicate the fabricated  $PN^{++}$ - junction such as doping concentrations at thermal equilibrium, junction depth, doping dependent and electron and hole mobilities and scattering rates, are used from our previous work [65]. The numerical model is designed to self-consistently solve for the device's position- and voltage-dependent charge carrier dynamics and the overall inhomogeneous local electron  $n(\vec{r}, V)$  and hole  $p(\vec{r}, V)$  concentration profiles, which are then used to calculate the inhomogeneous-, voltage-, and wavelength-dependent dielectric permittivity  $\epsilon(\vec{r}, \omega, V)$  of the entire device which is used to study the device's electromagnetic response including the TM-polarized reflectivity [65].

The reflectivity spectra of the current device is depicted in Figure 3A. A very good correspondence between experiment and theory is observed, thus indicating the validity of the

model for the unbiased device. The field profiles associated with the observed reflectivity features at  $\lambda \sim 7.3 \mu\text{m}$  and  $\lambda \sim 11.4 \mu\text{m}$  are provided in Figure 3B and 3C. The calculated local energy density associated with the dip positioned at  $\lambda \sim 11.4 \mu\text{m}$  in reflectivity spectra (see Figure 3B) clearly shows a localized profile located at the  $\text{PN}^{++}$  junction interface, suggesting the presence of a SPP mode. The mode profile related to the dip positioned at  $\lambda \sim 7.3 \mu\text{m}$  in the reflectivity spectrum, (see Figure 3C) does not show the characteristic profile of an SPP, and instead can be attributed to typical Fabry-Perot resonances formed between the interface and the top surface.

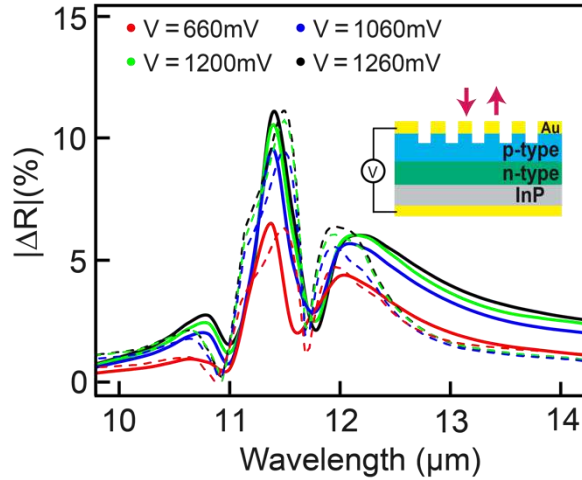


**Figure 3** (A) Transverse magnetic (TM) polarized reflectivity spectra of the SPPD (see insert) under zero bias. The experimental data (solid line) is compared to self-consistent electro-optic simulations (dotted line). (B-C) The local energy densities across the device calculated at the wavelengths corresponding to the two dips in the reflectivity spectra, i.e.,  $\lambda = 11.4 \mu\text{m}$  and  $\lambda = 7.3 \mu\text{m}$ . The local energy density profiles clearly show the excitation of SPPs at the  $\text{PN}^{++}$ - junction for an incident wavelength of  $\lambda = 11.4 \mu\text{m}$ .

To assess the device's steady state signal modulation, we have performed far field reflectivity studies both experimentally and numerically under four different forward voltages  $V \in$

$\{660mV, 1060mV, 1200mV, 1260mV\}$ . When evaluating the biased device's signal modulation experimentally, we used a setup similar to the one described for the unbiased device except that here the LIA is synchronized to a pulse generator which modulates the applied bias with a square wave at 10kHz and 50% Duty cycle. The interferogram generated in this experiment, when Fourier transformed, provides a measure of the modulation of the reflected signal as a function of wavelength. The modulation spectrum is then normalized to the sample's unbiased TM reflectivity, yielding the absolute change in reflectivity  $\Delta R(\lambda)$  as a function of wavelength. The results are depicted in Figure 4, where we have plotted the absolute change in reflectivity  $|\Delta R(\lambda, V)| = |R(\lambda, V) - R(\lambda, 0)|$ , for added clarity focusing on the wavelength window centered on the SPP coupling wavelength ( $\lambda = 11.4 \mu m$ ). We clearly observe an increase in the far field reflectivity with an increase in the external forward bias. Such behavior can be attributed to the injection of a significant number of minority carriers into the device  $P$ -layer. Such increase in the local minority carrier concentration alters the  $P$ -layer's permittivity, eventually creating conditions that prohibit the excitation of SPP modes at the  $PN^{++}$  - junction, leading to the OFF state of the device at sufficiently large applied forward bias. These results validate our initial hypothesis, i.e., in presence of external forward voltage, injection of charge carriers into the  $P$ -layer will be sufficient to electrically modulate the coupled SPP modes at the  $PN^{++}$  - junction. We note that the observed far-field reflectivity modulation  $\Delta R \approx 12\%$  of the presented device architecture is significantly higher compared to our previous studies [65], where a modest modulation of  $\Delta R \approx 1\%$  was demonstrated. This can be attributed to the specific placement of the bottom electrodes in the new device. Specifically, in our previous studies [65] the bottom electrodes are placed on either side of the  $PN^{++}$  Layer, whereas in the current architecture the bottom electrode is deposited at the bottom of the InP layer. Thus, changing the position of the bottom electrode can result in reducing

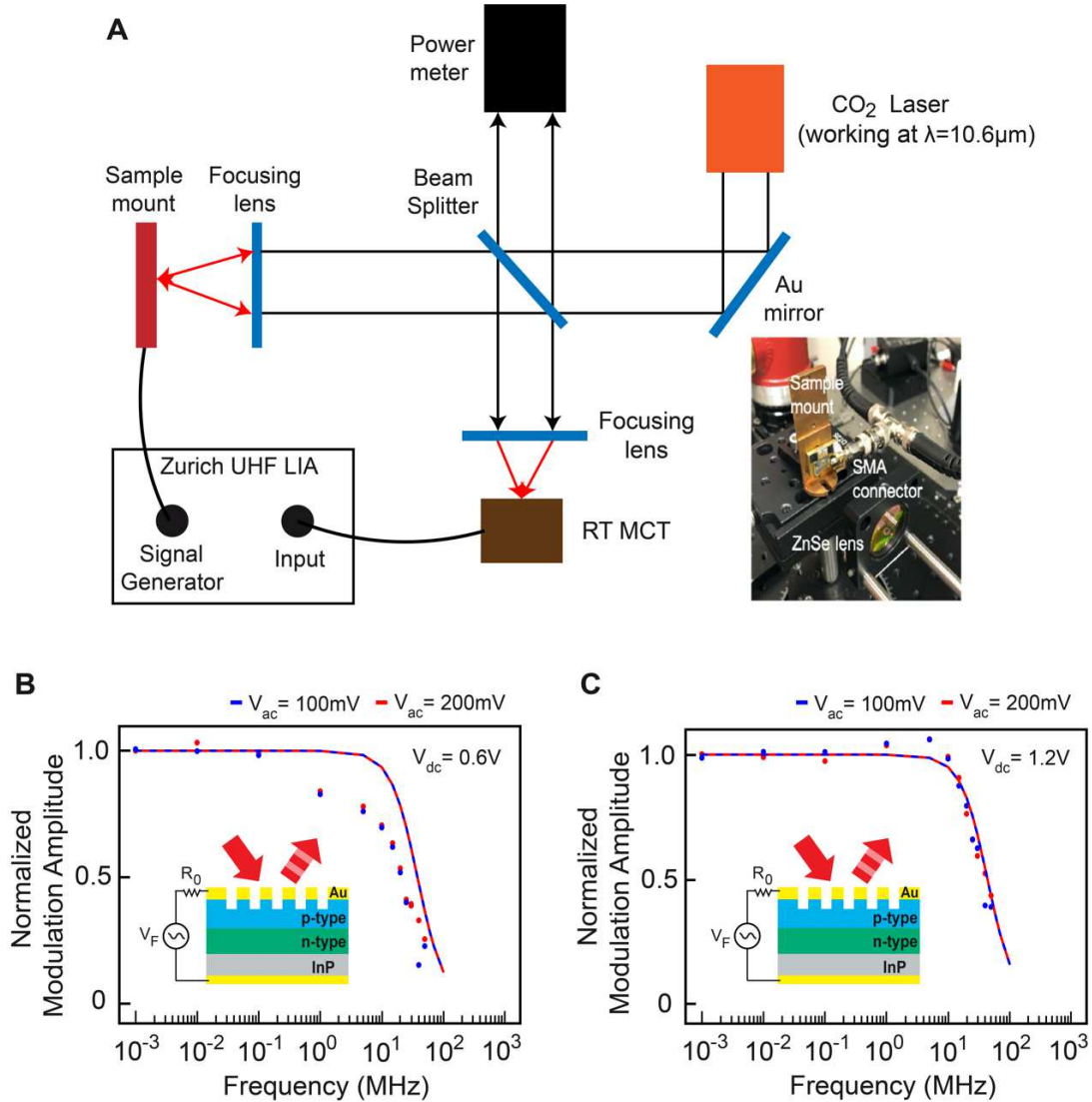
the effect of current spreading, providing a channel for larger concentration of minority carriers to be injected into the P-Layer resulting in a larger change in the P-layer permittivity and consequently the far-field reflectivity.



**Figure 4** Steady state SPPD reflectivity modulation. The absolute change in reflectivity is experimentally obtained under various forward bias voltages (solid lines) and compared to the self-consistent electro-optic simulations (dashed lines).

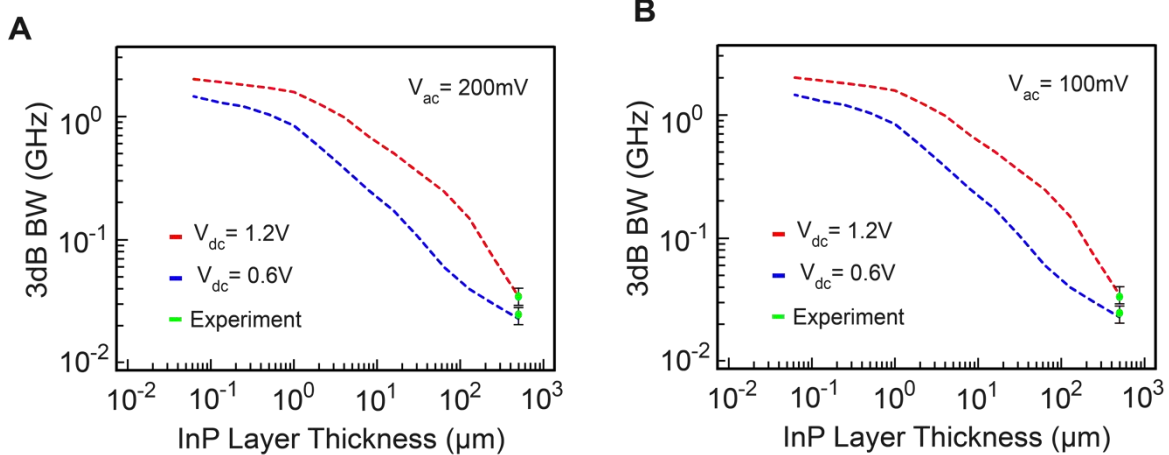
To assess the SPPD 3dB bandwidth, we have performed small signal transient analysis of the device through reflectivity measurements at a fixed input wavelength. Here, we used a CO<sub>2</sub> laser as a Continuous Wave (CW) source, tuned to an emission wavelength of  $\lambda = 10.61 \mu m$ , roughly corresponding to the short wavelength side of the feature, which will decrease the amplitude of modulation, but should not affect the achievable frequency of modulation (see Figure 4). The light from the laser was sent through a beam splitter with reflected light measured by a power meter and used as reference for the source power, in order to normalize for fluctuations in the laser power over time. The light transmitted through the beam splitter is focused on the sample

through a ZnSe lens with a 2-inch focal length. The sample was modulated by the output of a Zurich UHF lock-in amplifier (LIA), which was programmed to output an AC (sine wave) signal with varying DC offset;  $V_F = V_{dc} + V_{ac} \sin(\omega t)$  applied to the device. The amplitude of the applied voltage is limited by the series resistance ( $R_0$ ), which is the sum of the internal resistance of the function generator and the transmission line impedance. For our setup and low frequencies, we observed  $R_0 = 100\Omega$ . The reflected light was collected by the same ZnSe lens, incident on the beam splitter, with the reflected signal detected by a Boston Electronics PVM-10.6 room-temperature MCT detector (time constant 1.5ns). The output of the detector was then fed into the Zurich LIA, synchronized to the device-driving AC signal ( $V_F$ ). The complete setup is depicted in Figure 5A.



**Figure 5** SPPD frequency response. (A) Experimental setup schematic. Normalized far field modulation as a function of input driving AC small signal frequency, obtained under two sets of low frequency sinusoidal signal: (B)  $V_{dc} = 0.6\text{V}$  and  $V_{ac} = (100\text{mV}, 200\text{mV})$  (C)  $V_{dc} = 1.2\text{V}$  and  $V_{ac} = (100\text{mV}, 200\text{mV})$ . Experimental data is represented in dotted lines compared to the self-consistent electro-optic simulations (dashed lines). In the calculations the operation wavelength is set at  $\lambda = 10.61\mu\text{m}$ .

Figures 5B, and 5C depicts the experimentally measured frequency response of the device under four sets of sinusoidal input signals with driving frequencies varying from 1kHz up to 100MHz. The data indicates SPP modulation with 3dB bandwidths of 25MHz for DC voltage of 0.6V and 40MHz for DC voltage of 1.2V. The frequency response of the device is only weakly dependent on the small-signal AC voltage as expected. To explore the factors that determine the 3dB response of the device in higher details, we have compared the experimental data to numerical simulations (solid and dashed lines in Figure 5B and 5C). Overall, the theory agrees with the experimentally observed behavior both qualitative and quantitatively. We must note that the predicted and observed bandwidths are substantially lower compared to simulations performed by the authors elsewhere for shorter SPPDs [62, 63]. Indeed, this discrepancy is easily understood based on the fact that the fabricated device has a bottom InP layer with thickness  $d_3 = d_{InP} = 500 \mu m$  (see Figure 1) and doping concentration of  $1 \times 10^{18} cm^{-3}$ . From simulations we observe that this layer provides an estimated resistance of  $R_{InP} \sim 79 m\Omega$  translating into an additional voltage drop across the layer of the order of  $\Delta V_{InP} \sim 0.25V$  and additionally the time constant associated with the entire system that depends on the diffusion capacitance and differential resistance play a crucial role in the observed devices' reduced 3dB bandwidth. Hence, we expect that reducing the InP layer thickness should lead to substantial speed up of the SPPD switching speed.



**Figure 6** Numerical calculation of SPPD 3dB response times as function of the InP Layer thickness. In the calculations the device is operated using two sets of low frequency sinusoidal signal: (A)  $V_{ac} = 200mV$  and  $V_{dc} \in \{0.6V, 1.2V\}$  (B)  $V_{ac} = 100mV$  and  $V_{dc} \in \{0.6V, 1.2V\}$ . Experimental data is depicted in green dots. In the calculations the operation wavelength is set at  $\lambda = 10.61\mu m$ .

To better assess the SPPD 3dB response as a function of InP layer thickness, we have proceeded to numerically characterize the fabricated  $In_{0.53}Ga_{0.47}As$  based SPPD by theoretically decreasing the InP layer thickness. In the simulations we keep the same set of input voltages as those per Figure 5 and operated the device at the same incident wavelength of  $\lambda = 10.61\mu m$ . Our results are shown in Figure 6. As expected, the 3dB bandwidth is found to be inversely proportional with the InP thickness and then saturates for thin devices ( $d_{InP} < 1\mu m$ ) at about 2GHz. This is because the electron injection rate into the  $P$ -layer is inversely proportional to  $d_{InP}$  and proportional to the applied voltage bias, indicating that the optical modulation cutoff frequency is limited by the circuit speed. This distinctive behavior can be quantitatively explained using a simple drift-diffusion model of the electron dynamics within the drift-diffusion region. Overall,

our data shows that for a bare device, without the InP layer, 3dB bandwidth in excess of 2GHz can be achieved. Further improvement in the device's response times is expected by reducing the size of the drift-diffusion region (and varying the  $P$  and  $N^{++}$ - layers doping concentrations while keeping the SPP operation frequency within the mid-IR spectral range. Such type of optimization studies will be subject of future work.

## **Conclusion**

In conclusion we have performed time response analysis and optical characterization of an all-semiconductor based plasmonic switch, referred to as Surface Plasmon Polariton Diode (SPPD), comprising a grating-coupled, lattice-matched  $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$  degenerate  $PV^{++}$ - junction. Following, electrical control and temporal modulation of Surface Plasmon Polaritons (SPPs) at degenerate semiconductor interface is demonstrated within the mid-IR frequency range. The 3dB response times and the far-field reflectivity under the presence of a small signal AC bias was extensively studied experimentally and compared to numerical simulations, validating the proposed switching mechanism underlying the SPPD operation. Our data shows that the presented device architecture with 500  $\mu\text{m}$  InP layer can support 3dB bandwidths of 45MHz. Based on the excellent match between theory and experiment, we have performed small-signal transient studies of prospective SPPDs with various InP layer thickness. The data shows that the proposed SPPD architecture can provide 3dB bandwidths of up to 2GHz. Overall, the presented study indicates that degenerate semiconductor junctions can efficiently support excitation and control of SPP modes at mid-IR frequencies, an important step toward realization of prospective plasmonic circuit elements.

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**Author Contributions:**

R. V., Z. D., D. W. and D. A. G. contributed equally to executing the idea, analyzing the data and writing the manuscript. S. B. and A. B. grew the material.

**Competing Interests:**

The authors declare that they have no competing interests.

**Availability of Data and Materials:**

All data included in this article are available from the corresponding author upon reasonable request.

**Code Availability:**

All codes included in this article are available from the corresponding author upon reasonable request.

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